



LMG600 Series: New S-Channel v1.0

PRECISION IN POWER – THIS IS OUR GUIDELINE!

Our flagship channel - optimized for DC measurements

The growing use of direct current

While Westinghouse defeated Edison in the initial “War of Currents” more than a century ago, DC has come back vigorously in recent years. Both the dwindling away of fossil fuel reserves and an increased awareness of the impact of emissions on global climate have led to a surge in renewable sources of energy. Clean production of energy represents only half of the equation; the increasing adoption of electricity for locomotion makes sure that the consumption side stays low in emissions as well. The combination of photovoltaics with electromobility has proven to be very attractive and scalable.

S-Channel Features

- Superior AC & DC accuracy & stability
- Dedicated AC/DC ranges
- Automatic zero-adjustment
- Up to 1000 VAC, measurement category CAT III
- Up to 1500 VDC, measurement category CAT II

Admittedly, there is still potential for optimization when it comes to storage of electricity, but the growing market share of hybrid and electric cars has made research on efficient battery technologies more attractive and thus driven

innovation. With both production and utilization of electric energy going for DC, it is only natural to start thinking of DC grids for distribution as well. Put together, we see an impressive range of DC applications gaining momentum fast:

- **HVDC power superhighways:** Improving the efficiency of delivering electricity across long distances
- **PV arrays:** DC strings from residential to utility scale, reaching a system operating voltage of 1500 VDC to minimize BoS costs
- **DC charging infrastructure:** Fast charging station for electric vehicle operating on DC high power level
- **Electric vehicles:** Passenger cars, busses, vehicles for heavy goods transport and agriculture driven by electric drive trains
- **DC storage systems:** Sustainable use of solar energy with DC coupled storage systems on DC microgrids

From an instrumentation point of view, the shift from AC to DC calls for adaptations on the test & measurement side as well. After all, going for greener forms of energy does



not mean we can become careless when it comes to losses and efficiency. Even if we disregard the cost, there are other good reasons to avoid wasting energy. With charging points anything but ubiquitous yet and charging times considerably exceeding classic hydrocarbon refills, every additional mile squeezed out of the battery helps to make the transition from combustion to e-mobility more attractive. And what was valid for previous applications still holds true: the lower the efficiency, the more heat dissipated, the worse reliability and longevity of the product or component.

Why use a power analyzer for DC measurements?

The increased need for power measurements does not automatically translate to an increased need for power analyzers. Since DC power is easy to calculate – no need to account for phase shifts, power factors etc. – why use a power analyzer in the first place, instead of going for a cheaper multimeter? There are a few good reasons:

- **Usability:** Measuring and multiplying voltage and current separately can be cumbersome and error-prone. Power analyzers offer superior ease of use.
- **Derived values:** Often, the measured DC power needs to be set in relation to AC power (DC to AC, or vice versa) to determine efficiency. At this point, a genuine power analyzer becomes necessary anyway, so why not kill two birds with one stone?
- **Bandwidth:** The DC signals to be measured are rarely free of AC content. Typically, there is superimposed residual ripple stemming from the switching frequencies of DC-DC converters or rectifiers.

Depending on the phase relationship between voltage and current, this ripple might contribute to overall power. While the magnitude of the contribution might be minor, when looking at efficiencies >95 % it can become significant.



Figure 1: Rear Panel of the LMG671 equipped with 6 S-channels

How AC and DC measurements differ

Having established the continued need for the use of power analyzers under this new paradigm, we need to take a closer look at the specifics. Today's digital measurement instruments are based on the computation of voltage and current samples. The maximum signal amplitude needs to be correctly mapped to the A/D converters input range, otherwise the signal will be clipped and thus the measurement rendered invalid.

In the AC world, people typically think in RMS values, so in order to avoid clipping, the ratio of peak value to RMS value needs to be considered. This ratio is known as crest factor and can be given as $\sqrt{2} \approx 1.41$ for the usual sine-shaped grid voltages. Thus, a typical European RMS grid voltage of 230V maps to 325 V peak. However, the real peak value can be considerably higher once the signal is distorted. To spare the user mental gymnastics, it has been

established to use RMS values as nominal values to label measurement ranges. Thus, when measuring 230V grid voltage, the user simply has to select the 250V range without wasting any thoughts on the corresponding 400V peak value. Whereas voltage crest factors often are close to $\sqrt{2}$, current crest factors of up to 4 are anything but unusual. The difference between nominal and peak value of a measurement range needs to allow for those circumstances.

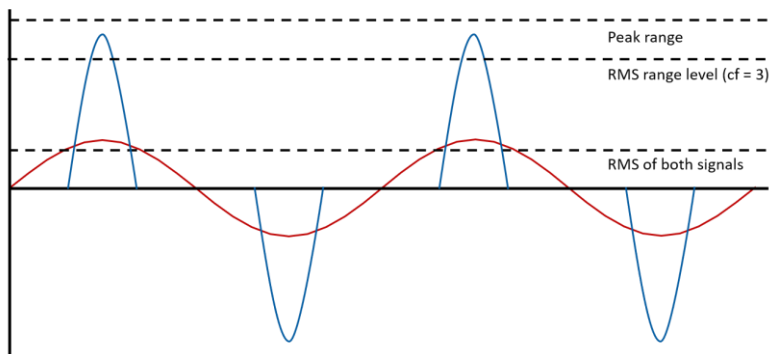


Figure 2: Comparison of two signals with same RMS value and different crest factors

Things are very different in the DC domain. RMS value and peak value are typically very close, crest factors are near 1. Even for a DC voltage up to 350V, choosing a 400V peak measuring range would not feel unnatural. The 50V headroom is more than sufficient to cover any ripple voltage to be expected. Choosing the 250V range (with naming conventions adopted from the AC world, as described above) to measure 350V would feel decidedly odd. Intuitively going for the next range – the 400V range with a peak value of 800V – would lead to very suboptimal utilization and unnecessarily increase measurement uncertainty.

This example illustrates that there is no easy way to reconcile the needs of AC and DC measurements when it comes to choosing meaningful names for measurement ranges. A naming convention that leads to an optimal utilization for DC signals will risk clipping the peak values of AC signals, conversely, measuring ranges with the desired safety margin required for AC will lead to suboptimal accuracy for DC.

The only way out: offering different range types for AC and DC signals.

Range
6.0 V
12.5 V
25.0 V
60.0 V
130.0 V
250.0 V
400.0 V
600.0 V
1.0 kV
Cancel

Figure 3: AC ranges selection

Range
10.0 V
20.0 V
45.0 V
90.0 V
180.0 V
360.0 V
720.0 V
1.0 kV
1.5 kV
Cancel

Figure 4: DC ranges selection

ZES ZIMMER’s new S-channel offers tailor-made measuring ranges for both AC and DC. When set to AC mode, the difference between nominal and peak values will allow for real-life crest factors. When set to DC mode, the nominal value will be closer to the maximum, suggesting a more intuitive choice of the range offering the best accuracy. In the above example, the 400V upper limit would correspond to a 250V range when set to AC, and a 360V range when set to DC.

Increased Measuring Range up to 1500 VDC between terminals

It is often desirable to increase the voltage levels in power systems to reduce currents, to minimize conductor cross-sections and decrease ohmic losses. A well-known example is the expansion of PV inverter voltage limits from 1000 VDC to 1500 VDC. As a consequence, solar PV plants can become more efficient despite reduced balance-of-system costs. Similar developments are taking place in the e-mobility sector. The need for faster charging leads to higher power levels, and current is inherently limited by available space and possibilities for heat dissipation. Voltage levels are therefore expected to rise beyond 1000 VDC in the near future, especially for heavy vehicles.

With 1500 VDC becoming mainstream for key applications, the input range of the S-channel has been expanded to accommodate those requirements. The Table 1 below depicts the measurement ranges for the jacks U* / U.

Nominal range AC / V	3	6	12.5	25	60	130	250	400	600	1000
Nominal range DC / V	5	10	20	45	90	180	360	720	1000	1500
Max. TRMS value / V	5.5	11	22	47	95	190	370	730	1010*	1510*
Max. peak value / V	6	12	25	50	100	200	400	800	1600	3200
Input impedance	2.69 MΩ ± 1% about 4 pF									
Overload capability	U _{AC} = 1000 V + 10% continuously U _{AC} = 1500 V for 1 s U _{DC} = 1500 V + 10% continuously U = 2500 V for 20 ms, transient									
Capacity against earth	about 90 pF									

* See specification of overload capability, max. measurable RMS values, max. isolation voltage and the corresponding warnings in the manual

Table 1: Measurement ranges for voltage input jacks U*/U

Accuracy Specifications

S channel Accuracy	± (% of measured value + % of maximum peak value)
	DC ^e
Voltage U*	0.02+0.04
Voltage U _{SENSOR}	0.02+0.04 ^d
Current I* 5 mA...5 A range AC, 10 mA...8 A range DC	0.02+0.04
Current I* 10 A...32 A range AC, 15 A...32 A range DC	0.02+0.1 ^f
Current I _{SENSOR}	0.02+0.04 ^d
Active Power	$\Delta P_{DC} = \pm(\Delta U_{DC} \cdot I_{DC} + \Delta I_{DC} \cdot U_{DC})$ Description of the used formula symbols, see ACCURACY SPECIFICATIONS in the manual.

Table 2: L60-CH-S2: DC Accuracy

f: Additional accuracy specification in the 10 A ... 32 A range AC or 15 A ... 32 A range DC: $\pm \frac{80 \mu A}{A^2} \cdot I_{trms}^2$
 d: Accuracy specification is valid with activated signal filter 15 kHz or 150 kHz
 e: Accuracy specification is valid with activated automatic zero adjustment, max. 24 h after last change of the measuring range in the current measurement channel, temperature change after change of the measuring range max. ±1 °C, max. 30 days after persistent zero adjustment in the voltage measurement channel (see ZERO ADJUSTMENT in the manual)

S channel Accuracy	± (% of measured value + % of maximum peak value)								
	0.05 Hz ... 45 Hz 65 Hz ... 3 kHz	45 Hz ... 65 Hz	3 kHz ... 10 kHz	10 kHz ... 50 kHz	50 kHz ... 100 kHz	100 kHz ... 500 kHz	500 kHz ... 1 MHz	1 MHz ... 2 MHz	2 MHz ... 10 MHz
Voltage U*	0.015+0.03	0.01+0.02	0.03+0.06	0.2+0.4		0.5+1.0	0.5+1.0	f/1 MHz*1.5 + f/1 MHz*1.5	
Voltage U _{SENSOR}	0.015+0.03	0.01+0.02	0.03+0.06	0.2+0.4		0.4+0.8	0.4+0.8	f/1 MHz*0.7 + f/1 MHz*1.5	
Current I* 5 mA...5 A range AC, 10 mA...8 A range DC	0.015+0.03	0.01+0.02	0.03+0.06	0.2+0.4		0.5+1.0	0.5+1.0	f/1 MHz*1.0 + f/1 MHz*2.0	-
Current I* 10 A...32 A range AC, 15 A...32 A range DC	0.015+0.03 ^f	0.01+0.02 ^f	0.1+0.2 ^f	0.3+0.6 ^f	f/100 kHz*0.8 + f/100 kHz*1.2 ^f		-		
Current I _{SENSOR}	0.015+0.03	0.01+0.02	0.03+0.06	0.2+0.4		0.4+0.8	0.4+0.8	f/1 MHz*0.7 + f/1 MHz*1.5	
Active Power U*/I* 5 mA...5 A range AC, 10 mA...8 A range DC	0.024+0.03	0.015+0.01	0.048+0.06	0.32+0.4		0.8+1.0	0.8+1.0	f/1 MHz*2.0 + f/1 MHz*1.8	-
Active Power U*/I* 10 A...32 A range AC, 15 A...32 A range DC	0.024+0.03 ^g	0.015+0.01 ^g	0.104+0.13 ^g	0.4+0.5 ^g	f/100 kHz*0.8 + f/100 kHz*0.8 ^g	f/100 kHz*1.0 + f/100 kHz*1.1 ^g	-		
Active Power U*/I _{SENSOR}	0.024+0.03	0.015+0.01	0.048+0.06	0.32+0.4		0.72+0.9	0.72+0.9	f/1 MHz*1.8 + f/1 MHz*1.5	
Active Power U _{SENSOR} /I*	0.024+0.03	0.015+0.01	0.048+0.06	0.32+0.4		0.72+0.9	0.72+0.9	f/1 MHz*1.4 + f/1 MHz*1.8	-
Active Power U _{SENSOR} /I* 10 A...32 A range AC, 15 A...32 A range DC	0.024+0.03 ^g	0.015+0.01 ^g	0.104+0.13 ^g	0.4+0.5 ^g	f/100 kHz*0.8 + f/100 kHz*0.8 ^g	f/100 kHz*1.0 + f/100 kHz*1.1 ^g	-		
Active Power U _{SENSOR} /I _{SENSOR}	0.024+0.03	0.015+0.01	0.048+0.06	0.32+0.4		0.64+0.8	0.64+0.8	f/1 MHz*1.1 + f/1 MHz*1.5	

Table 3: L60-CH-S2: AC Accuracy 0.05 Hz ... 10 MHz

f: Additional accuracy specification in the 10 A ... 32 A range AC or 15 A ... 32 A range DC: $\pm \frac{80 \mu A}{A^2} \cdot I_{rms}^2$

g: Additional accuracy specification in the 10 A ... 32 A range AC or 15 A ... 32 A range DC: $\pm \frac{80 \mu A}{A^2} \cdot I_{rms}^2 \cdot U_{rms}$

Contact us

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